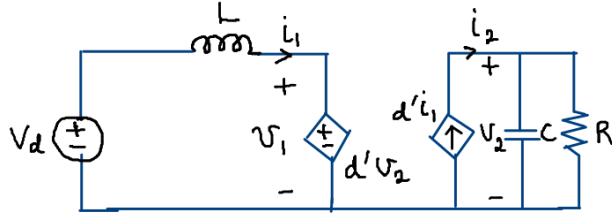


**Question 1**

The averaged circuit model of an ideal boost converter is shown in Figure Q1. The boost converter has  $L = 75 \mu\text{H}$ ,  $C = 330 \mu\text{F}$ , input voltage,  $v_d = 18 \text{ V}$ , output voltage,  $v_o = 30 \text{ V}$ , load resistance,  $R = 30 \Omega$ , and switching frequency  $f_s = 100 \text{ kHz}$ . The circuit operates in continuous conduction mode.

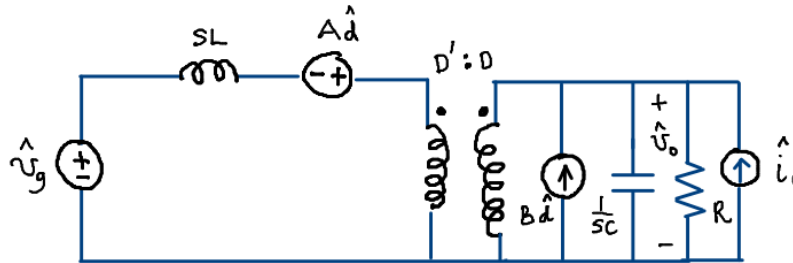


**Figure Q1**

- (i) By doing perturbation and linearization on the averaged circuit model, obtain AC small-signal model and DC steady-state model. [5 marks]
- (ii) Analyze DC steady-state model to determine all bias point constants. [5 marks]

**Question 2**

Analyze AC small signal model to obtain control to output transfer function,  $\frac{\hat{v}_o}{\hat{d}}(s)$  for the AC small signal circuit in Figure Q2. A and B are circuit constants. [4 marks]



**Figure Q2**

**Question 3**

A buck converter has  $L = 35 \mu\text{H}$ ,  $C = 440 \mu\text{F}$ , equivalent series resistance of capacitor,  $R_{ESR} = 25 \text{ m}\Omega$ , the input voltage,  $V_d = 18 \text{ V}$ , the output voltage,  $v_o = 12 \text{ V}$ , load resistance,  $R = 6 \Omega$ , and the switching frequency  $f_s = 100 \text{ kHz}$ . The PWM has the sawtooth peak  $V_m = 2 \text{ V}$  and the error amplifier has  $V_{ref} = 2 \text{ V}$ . The circuit operates in continuous conduction mode.

It is desired to design a type-3 error amplifier, as shown in the **Appendix B**, based on pole-zero placement, that will give the crossover frequency of 10 kHz. The poles and zeros of the error amplifier are placed as follows: (i) the two zeros are placed at resonant frequency,  $f_o$ ; (ii) the first and second poles are placed at  $f_{zSER}$  and  $0.75f_s$ , respectively.

- (i) Determine the magnitude in dB and phase in degrees of the loop gain at the crossover frequency, including error amplifier (with  $\omega_i = 1$ ). [6 marks]
- (ii) What is the gain of the error amplifier required at the crossover frequency? [2 marks]
- (iii) Determine all resistance and capacitance values of the type-3 error amplifier (see Appendix A). [4 marks]

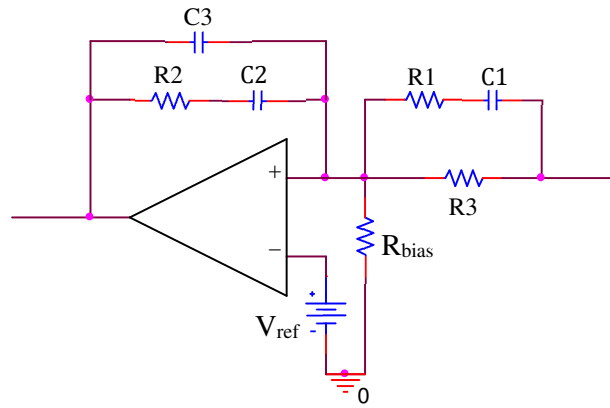
## Potentially Useful Formula

Transfer Function	With $s = j\omega$	Gain	Phase
$1 + \frac{s}{\omega_z}$	$1 + j\frac{\omega}{\omega_z}$	$\sqrt{1 + \left(\frac{\omega}{\omega_z}\right)^2}$	$\tan^{-1}\left(\frac{\omega}{\omega_z}\right)$
$1 - \frac{s}{\omega_z}$	$1 - j\frac{\omega}{\omega_z}$	$\sqrt{1 + \left(\frac{\omega}{\omega_z}\right)^2}$	$-\tan^{-1}\left(\frac{\omega}{\omega_z}\right)$
$\frac{1}{1 + \frac{s}{\omega_p}}$	$\frac{1}{1 + j\frac{\omega}{\omega_p}}$	$\frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_p}\right)^2}}$	$-\tan^{-1}\left(\frac{\omega}{\omega_p}\right)$
$\frac{1}{1 + \frac{s}{Q\omega_o} + \frac{s^2}{\omega_o^2}}$	$\frac{1}{1 - \left(\frac{\omega}{\omega_o}\right)^2 + j\frac{\omega}{Q\omega_o}}$	$\frac{1}{\sqrt{\left[1 - \left(\frac{\omega}{\omega_o}\right)^2\right]^2 + \left(\frac{\omega}{Q\omega_o}\right)^2}}$	$-\tan^{-1}\left(\frac{\omega/Q\omega_o}{1 - \left(\frac{\omega}{\omega_o}\right)^2}\right)$

Converter	Control-to-output transfer function, $\frac{\hat{v}_o}{\hat{d}}$	Parameters definition
Buck	$g_{do} \frac{\left(1 + \frac{s}{\omega_{zESR}}\right)}{1 + \frac{s}{Q\omega_o} + \frac{s^2}{\omega_o^2}}$	$g_{do} = V_d$ ; $\omega_o = \frac{1}{\sqrt{LC}}$ $\omega_{zESR} = \frac{1}{rC}$ ; $Q = \frac{R}{\omega_o L}$
Boost	$g_{do} \frac{\left(1 - \frac{s}{\omega_{zRHP}}\right)\left(1 + \frac{s}{\omega_{zESR}}\right)}{1 + \frac{s}{Q\omega_o} + \frac{s^2}{\omega_o^2}}$	$g_{do} = \frac{V_d}{(1-D)^2}$ ; $\omega_o = \frac{1}{\sqrt{L_{eq}C}}$ $\omega_{zESR} = \frac{1}{rC}$ ; $\omega_{zRHP} = \frac{R}{L_{eq}}$ $Q = \frac{R}{\omega_o L_{eq}}$ ; $L_{eq} = \frac{L}{(1-D)^2}$
Buck-boost	$g_{do} \frac{\left(1 - \frac{s}{\omega_{zRHP}}\right)\left(1 + \frac{s}{\omega_{zESR}}\right)}{1 + \frac{s}{Q\omega_o} + \frac{s^2}{\omega_o^2}}$	$g_{do} = \frac{V_d}{(1-D)^2}$ ; $\omega_o = \frac{1}{\sqrt{L_{eq}C}}$ $\omega_{zESR} = \frac{1}{rC}$ ; $\omega_{zRHP} = \frac{R}{DL_{eq}}$ $Q = \frac{R}{\omega_o L_{eq}}$ ; $L_{eq} = \frac{L}{(1-D)^2}$

## Appendix B

## Pole-zero placement for type 3 error amplifier



1. Calculate the gain,  $A_{co}$  (in dB), and the phase,  $P_{co}$  (in degree), of the loop gain at the cross over frequency,  $f_{co}$ . For the error amplifier,  $\omega_i = 1$ .
2. Calculate the error amplifier gain,  $\omega_i$ , required:

$$\omega_i = 10^{\frac{-A_{co}}{20}}$$

3. Calculate capacitances and resistances consecutively:

$$R_3 = 10 \text{ k}\Omega$$

$$C_3 = \frac{f_{z2}}{(\omega_i R_3 f_{p2})}$$

$$C_2 = C_3 \left( \frac{f_{p2}}{f_{z2}} - 1 \right)$$

$$R_2 = \frac{1}{2\pi f_{z2} C_2}$$

$$R_1 = \frac{R_3}{\left( \frac{f_{p1}}{f_{z1}} - 1 \right)}$$

$$C_1 = \frac{1}{2\pi f_{p1} R_1}$$

$$R_{bias} = \frac{V_{ref}}{V_o - V_{ref}} R_3$$