

Test #2: Solution

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Dummy unit: $\Omega \equiv 1$ $A \equiv 1$ $V \equiv 1$ $W \equiv 1$ $kW \equiv 1 \cdot 10^3 \cdot W$ $Hz \equiv 1$
 $Nm \equiv 1$ $rpm \equiv 1$

Q1: DC Machine - speed of the motor under full load condition

Under full load: $P_{\text{Rated}} := 10.0kW$ $E_{a\text{Rated}} := 100V$ $V_t := 100V$ $R_a := 0.1\Omega$

$$I_{a\text{FL}} := \frac{P_{\text{Rated}}}{E_{a\text{Rated}}} \quad I_{a\text{FL}} = 100 \text{ A}$$

$$E_{a\text{FL}} := V_t - I_{a\text{FL}} \cdot R_a \quad E_{a\text{FL}} = 90 \text{ V}$$

Under no load: Given: $E_a = 99V$ at No load $\omega_{\text{NL}} := 1000\text{rpm}$

Therefore, $E_{a\text{NL}} := 99V$

R_f and rotational loss

3 marks

For $E_a := 98V$ $I_f := 0.95A$

$$R_f := \frac{V_t}{I_f} \quad R_f = 105.263 \Omega$$

$$I_a := \frac{V_t - E_a}{R_a} \quad I_a = 20$$

Rotational loss: $P_{\text{loss}} := E_a \cdot I_a$ $P_{\text{loss}} = 1.96 \times 10^3 \text{ W}$

(a) With armature reaction, 5.8% reduction in flux due to armature reaction.

3 marks

$$\Phi_{\text{FL}} = \left(1 - \frac{5.8}{100}\right) \cdot \Phi_{\text{NL}} \quad \Phi_{\text{FL}} = 0.942 \cdot \Phi_{\text{NL}}$$

$$\frac{E_{a\text{FL}}}{E_{a\text{NL}}} = \frac{0.942 \cdot \omega_{\text{FL}}}{\omega_{\text{NL}}} \quad \text{Therefore, } \omega_{\text{FL}} := \frac{E_{a\text{FL}}}{E_{a\text{NL}}} \cdot \frac{\omega_{\text{NL}}}{0.942} \quad \omega_{\text{FL}} = 965.065 \text{ rpm}$$

(b) With armature reaction:

3 marks

For cumulative compound motor,

$$I_{f_eff} = I_f - I_{f_AR} + \frac{N_{sr}}{N_f} \cdot I_t$$

$$I_{f_AR} := 0.15A$$

$$I_f := 0.95A$$

$$\frac{\omega_C}{\omega_D} = \frac{E_C}{E_D}$$

$$\omega_C := 1000\text{rpm}$$

$$\omega_D := 818\text{rpm}$$

$$E_D := E_{aFL}$$

$$E_D = 90V$$

$$E_C := \frac{\omega_C}{\omega_D} \cdot E_D$$

$$E_C = 110.024V$$

From the graph, when

$$E_C = 110V$$

$$I_f = 1.4A$$

(Point C)

$$I_{f_eff} = I_f - I_{f_AR} + \frac{N_{sr}}{N_f} \cdot I_t$$

$$I_{f_eff} := 1.4A$$

$$I_{f_AR} := 0.15$$

$$N_f := 800$$

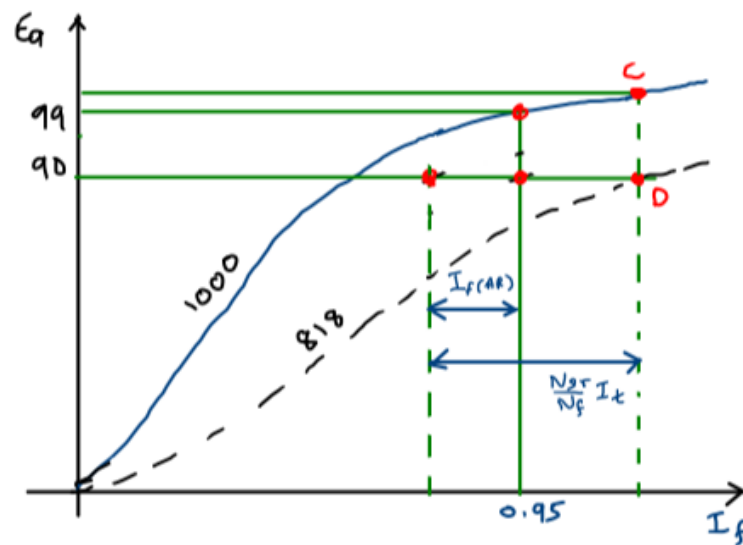
$$I_t := I_{aFL} + I_f$$

$$I_{aFL} = 100$$

$$I_f = 0.95$$

$$N_{sr} := (I_{f_eff} - I_f + I_{f_AR}) \cdot \frac{N_f}{I_t}$$

$$N_{sr} = 4.755$$



(c) From (a)

$$\omega_F := 965$$

$$E_F := 90V$$

3 marks

$$\omega_G := 1000$$

$$E_G = \text{unknown}$$

$$E_G := \frac{\omega_G}{\omega_F} \cdot E_F$$

$$E_G = 93.264V$$

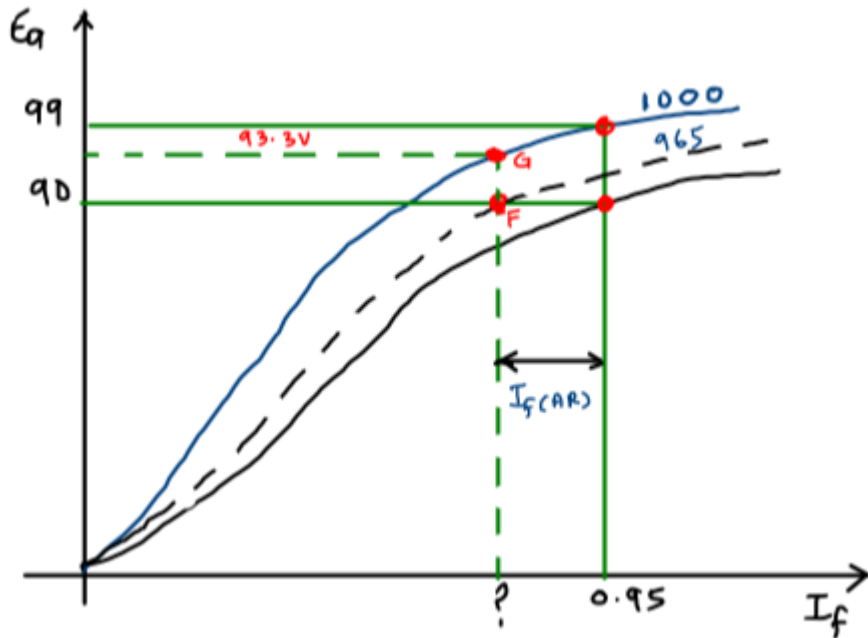
From the graph,

$$\text{for } E_G = 93.264$$

$$I_{f_eff} := 0.775$$

and $I_f = 0.95$

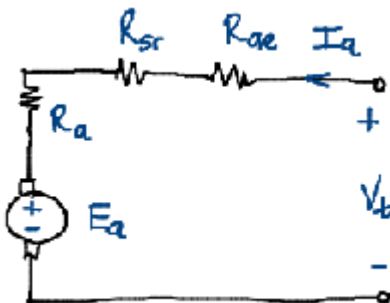
$$I_{f_AR} := I_f - I_{f_eff} \quad I_{f_AR} = 0.175 \text{ A}$$



Q2: DC Series Motor - Speed control of DC series motor by varying R_a .

$$V_t := 330\text{V} \quad R_a := 0.6\Omega \quad R_{sr} := 0.4\Omega$$

An Equivalent circuit of the series DC motor



(a) To determine key quantities at the operating point 1.

$$\text{Operation at point 1:} \quad \omega_{m1} := 500 \cdot \text{rpm} \quad I_{a1} := 28\text{A} \quad R_{ae1} := 0$$

Therefore,

$$E_{a1} := V_t - I_{a1} \cdot (R_a + R_{sr} + R_{ae1}) \quad E_{a1} = 302 \text{ V}$$

$$P_1 := E_{a1} \cdot I_{a1} \quad P_1 = 8.456 \text{ kW}$$

$$T_1 := \frac{E_{a1} \cdot I_{a1}}{\frac{\omega_{m1}}{60} \cdot 2\pi} \quad T_1 = 161.498 \text{ Nm}$$

3 marks

(b) To determine key quantities at the operating point 2.

Operation at point 2: $\omega_{m2} := 400 \cdot \text{rpm}$

Since the load torque is proportional to square root of the motor speed,

$$T_2 := \left(\frac{\omega_{m2}}{\omega_{m1}} \right) \cdot T_1 \quad T_2 = 129.198$$

To find K_{sr} : $T_1 = K_{sr} \cdot I_{a1}^2 \quad K_{sr} := \frac{T_1}{I_{a1}^2} \quad K_{sr} = 0.206$

$$I_{a2} := \sqrt{\frac{T_2}{K_{sr}}} \quad I_{a2} = 25.044 \text{ A}$$

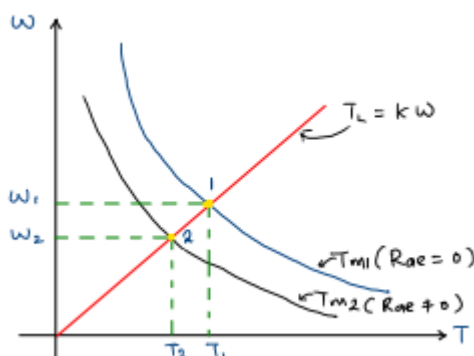
$$E_{a2} := K_{sr} \cdot I_{a2} \cdot \omega_{m2} \cdot \frac{2\pi}{60} \quad E_{a2} = 216.094 \text{ V}$$

$$R_{ae2} := \frac{V_t - E_{a2}}{I_{a2}} - (R_a + R_{sr}) \quad R_{ae2} = 3.548 \Omega$$

$$P_2 := E_{a2} \cdot I_{a2} \quad P_2 = 5.412 \text{ kW}$$

3 marks

(c) Speed-torque characteristics



2 marks

Q3: Induction Machine - power flow

$$V_L := 415\text{V} \quad I_p := 90\text{A} \quad P_{ag} := 53\text{kW} \quad N_r := 700\text{rpm} \quad p := 8 \quad f := 50\text{Hz}$$

$$\Delta\text{-connected} \quad P_{rotat} := 1\text{kW} \quad P_{stator} := 1.2\text{kW} \quad \eta := \frac{85}{100}$$

i. $N_s := \frac{120 \cdot f}{p} \quad N_s = 750\text{rpm}$ 1 mark

$$s := \frac{N_s - N_r}{N_s} \quad s = 0.067$$

ii. $P_m := (1 - s) \cdot P_{ag} \quad P_m = 49.467\text{kW}$ 1 mark

iii. $P_m = P_o + P_{rotat}$ 1 mark

$$P_o := P_m - P_{rotat} \quad P_o = 48.467\text{kW}$$

iv. $P_{rotor} := s \cdot P_{ag} \quad P_{rotor} = 3.533\text{kW}$ 1 mark

v. $\eta = \frac{P_o}{P_{in}}$ 1 mark

$$P_{in} := \frac{P_o}{\eta} \quad P_{in} = 57.02\text{kW}$$

vi. $P_{in} = P_{ag} + P_{stator}$ 1 mark

$$P_{stator} := P_{in} - P_{ag} \quad P_{stator} = 4.02\text{kW}$$

vii. $P_{loss} := P_{in} - P_o \quad P_{loss} = 8.553\text{kW}$

viii. $I_L := \sqrt{3} \cdot I_p \quad I_L = 155.885\text{A}$ 1 mark

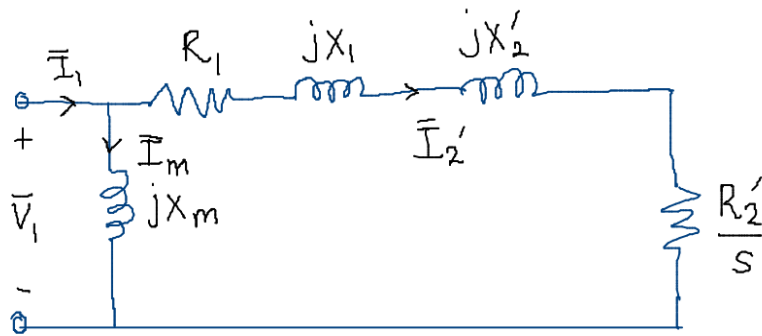
$$P_{in} = \sqrt{3} \cdot V_L \cdot I_L \cdot \text{pf} \quad \text{pf} := \frac{P_{in}}{\sqrt{3} \cdot V_L \cdot I_L} \quad \text{pf} = 0.509 \quad \text{lagging}$$

Q4: Induction Machine - Equivalent Circuit Analysis

$$R_1 := 0.5\Omega \quad R_2 := 1.2\Omega \quad X_1 := 2\Omega \quad X_2 := 1.0\Omega \quad X_m := 60\Omega$$

$$V_L := 460\text{V} \quad N_r := 970\text{rpm} \quad p := 6 \quad f := 50\text{Hz} \quad \Delta \text{ connected}$$

We use an approximate equivalent circuit. The calculation uses per phase quantities.



Connection Type:
Delta

$$V_1 := V_L \quad V_1 = 460 \text{ V} \quad N_s := \frac{120f}{p} \quad N_s = 1 \times 10^3 \text{ rpm}$$

i. $N_s := \frac{120 \cdot f}{p} \quad N_s = 1 \times 10^3 \text{ rpm} \quad s := \frac{N_s - N_r}{N_s} \quad s = 0.03$ 2 marks

slip speed, $N_{\text{slip}} := N_s - N_r \quad N_{\text{slip}} = 30 \text{ rpm}$

Under full-load condition, i.e. when $s_{\text{FL}} := s \quad s_{\text{FL}} = 0.03$

ii. $I_2 := \frac{V_1}{R_1 + \frac{R_2}{s} + j \cdot (X_1 + X_2)}$ **mag** $|I_2| = 11.327 \text{ A}$ **phase** $\arg(I_2) = -4.236 \text{ deg}$ 2 marks

$I_m := \frac{V_1}{j \cdot X_m}$ **mag** $|I_m| = 7.667 \text{ A}$ **phase** $\arg(I_m) = -90 \text{ deg}$

$I_1 := I_2 + I_m$ **mag** $|I_1| = 14.139 \text{ A}$ **phase** $\arg(I_1) = -36.972 \text{ deg}$

The power factor, $\text{pf} = \cos(\theta)$

$\text{pf} := \cos(\arg(I_1))$ pf = 0.799 lagging

iii. $P_{\text{ag}} := (|I_2|)^2 \frac{R_2}{s}$ P_{ag} = 5.132 kW per phase 2 marks

$P_{\text{rotor}} := s \cdot P_{\text{ag}} \quad P_{\text{rotor}} = 153.961 \text{ W}$ per phase

iv. $P_m := (1 - s) \cdot P_{\text{ag}} \quad P_m = 4.978 \text{ kW}$ per phase 1 mark

v. $P_m = P_o + P_{\text{rotat}}$ $P_{\text{rotat}} := \frac{900}{3}$ per phase **2 marks**

$P_o := P_m - P_{\text{rotat}}$ $P_o = 4.678 \text{ kW}$ per phase

$P_{\text{in}} := |V_1| \cdot |I_1| \cdot \text{pf}$ $P_{\text{in}} = 5.196 \text{ kW}$ per phase

vi. Efficiency, $\eta := \frac{P_o}{P_{\text{in}}}$ $\eta = 90.029 \%$ **1 mark**