

Test #2: Solution

Version: 2/4Jan17

Dummy unit: $\Omega \equiv 1$ $A \equiv 1$ $V \equiv 1$ $W \equiv 1$ $kW \equiv 1 \cdot 10^3 \cdot W$ $Hz \equiv 1$
 $Nm \equiv 1$ $rpm \equiv 1$

Q1: DC Machine - speed of the motor under full load condition

Under full load: $P_{\text{Rated}} := 10.0kW$ $E_{a\text{Rated}} := 100V$ $V_t := 100V$ $R_a := 0.1\Omega$

$$I_{a\text{FL}} := \frac{P_{\text{Rated}}}{E_{a\text{Rated}}} \quad I_{a\text{FL}} = 100 \text{ A}$$

$$E_{a\text{FL}} := V_t - I_{a\text{FL}} \cdot R_a \quad E_{a\text{FL}} = 90 \text{ V}$$

Under no load: Given: $E_a = 99V$ at No load $\omega_{\text{NL}} := 1000rpm$

Therefore, $E_{a\text{NL}} := 99V$

(a) With armature reaction, $\phi_{\text{FL}} = 0.925\phi_{\text{NL}}$ (7.5% reduction in flux due to armature reaction)

$$\frac{E_{a\text{FL}}}{E_{a\text{NL}}} = \frac{0.925 \cdot \omega_{\text{FL}}}{\omega_{\text{NL}}} \quad \text{Therefore,} \quad \omega_{\text{FL}} := \frac{E_{a\text{FL}}}{E_{a\text{NL}}} \cdot \frac{\omega_{\text{NL}}}{0.925} \quad \omega_{\text{FL}} = 982.801 \text{ rpm}$$

3 marks

(b) With armature reaction: $I_{f_AR} := 0.1A$

$$I_f := 0.95A \quad I_{f_eff} := I_f - I_{f_AR} \quad I_{f_eff} = 0.85A$$

From the graph, when $I_f = 0.85A$ $E_a = 96V$ (Point D)

At the point C, $E_a = 90V$

Now, we know that:

$$E_{aD} := 96V \quad E_{aC} := 90V \quad \omega_D := 1000rpm$$

Points C and D are related using:

$$\frac{\omega_D}{\omega_C} = \frac{E_{aD}}{E_{aC}} \quad \text{and} \quad \omega_C := \frac{E_{aC}}{E_{aD}} \cdot \omega_D \quad \omega_C = 937.5 \text{ rpm}$$

3 marks

(c) With armature reaction: $\phi_{\text{FL}} = 0.925\phi_{\text{NL}}$

$$\omega_F := 1000 \text{ rpm}$$

We need to find E_F

$$\omega_E := 982.801 \text{ rpm} \quad \text{From the solution (a)}$$

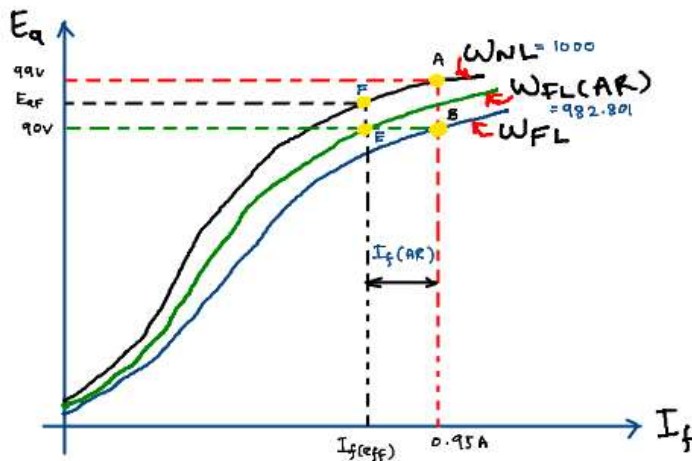
$$E_E := 90 \text{ V}$$

$$E_F := \frac{\omega_F}{\omega_E} \cdot E_E \quad E_F = 91.575 \text{ V}$$

From the graph, $E_a = 91.575 \text{ V}$ $I_f = 0.72 \text{ A}$ i. e. I_f effective

$$I_{f_AR} = I_f - I_{f_eff} = 0.95 - 0.72 = 0.23 \text{ A}$$

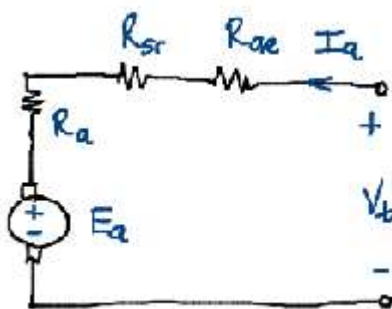
2 marks



Q2: DC Series Motor - Speed control of DC series motor by varying R_a .

$$V_t := 350 \text{ V} \quad R_a := 0.5 \Omega \quad R_{sr} := 0.3 \Omega$$

An Equivalent circuit of the series DC motor



(a) To determine key quantities at the operating point 1.

$$\text{Operation at point 1:} \quad \omega_{m1} := 600 \cdot \text{rpm} \quad I_{a1} := 30 \text{ A} \quad R_{ae1} := 0$$

Therefore,

$$E_{a1} := V_t - I_{a1} \cdot (R_a + R_{sr} + R_{ae1})$$

$$E_{a1} = 326 \text{ V}$$

$$P_1 := E_{a1} \cdot I_{a1} \quad P_1 = 9.78 \text{ kW}$$

$$T_1 := \frac{E_{a1} \cdot I_{a1}}{\frac{\omega_{m1}}{60} \cdot 2\pi} \quad T_1 = 155.654 \text{ Nm}$$

3 marks

(b) To determine key quantities at the operating point 2.

$$\text{Operation at point 2:} \quad \omega_{m2} := 500 \cdot \text{rpm}$$

Since the load torque is proportional to square root of the motor speed,

$$T_2 := \left(\frac{\omega_{m2}}{\omega_{m1}} \right)^{2.25} \cdot T_1 \quad T_2 = 103.276 \text{ Nm}$$

$$\text{To find } K_{sr}: \quad T_1 = K_{sr} \cdot I_{a1}^2 \quad K_{sr} := \frac{T_1}{I_{a1}^2} \quad K_{sr} = 0.173$$

$$I_{a2} := \sqrt{\frac{T_2}{K_{sr}}} \quad I_{a2} = 24.437 \text{ A}$$

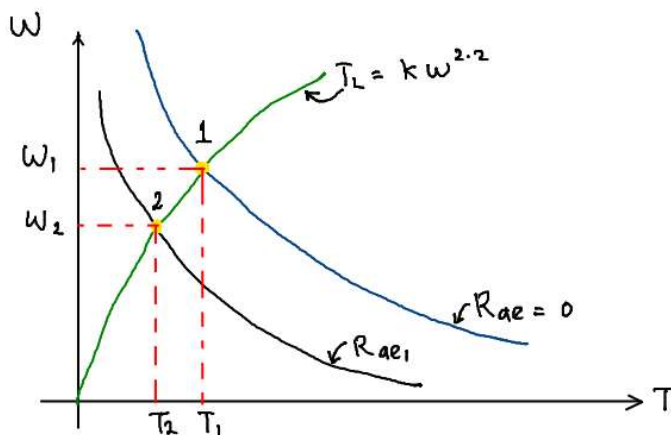
$$E_{a2} := K_{sr} \cdot I_{a2} \cdot \omega_{m2} \cdot \frac{2\pi}{60} \quad E_{a2} = 221.288 \text{ V}$$

$$R_{ae2} := \frac{V_t - E_{a2}}{I_{a2}} - (R_a + R_{sr}) \quad R_{ae2} = 4.467 \Omega$$

$$P_2 := E_{a2} \cdot I_{a2} \quad P_2 = 5.408 \text{ kW}$$

3 marks

(c) Speed-torque characteristics



2 marks

Q3: Induction Machine - power flow

$$V_L := 380V \quad I_L := 96A \quad P_{out} := 47.5kW \quad N_r := 575rpm \quad p := 10 \quad f := 50Hz$$

$$\Delta\text{-connected} \quad P_{rotat} := 1kW \quad \eta := 0.92$$

$$N_s := \frac{120 \cdot f}{p} \quad N_s = 600 \text{ rpm}$$

$$s := \frac{N_s - N_r}{N_s} \quad s = 0.042$$

i. $P_m := P_{out} + P_{rotat} \quad P_m = 48.5kW$ 1 mark

ii. $P_{ag} := \frac{P_m}{(1-s)} \quad P_{ag} = 50.609kW$ 1 mark

iii. $P_{rotor} := s \cdot P_{ag} \quad P_{rotor} = 2.109kW$ 1 mark

iv. $P_{in} := \frac{P_{out}}{\eta} \quad P_{in} = 51.63kW$ 1 mark

v. $P_{stator} := P_{in} - P_{ag} \quad P_{stator} = 1.022kW$ 1 mark

vi. $P_{Losses} := P_{rotat} + P_{rotor} + P_{stator} \quad P_{Losses} = 4.13kW$ 1 mark

vii. $P_{losses} := P_{in} - P_{out} \quad P_{losses} = 4.13kW$

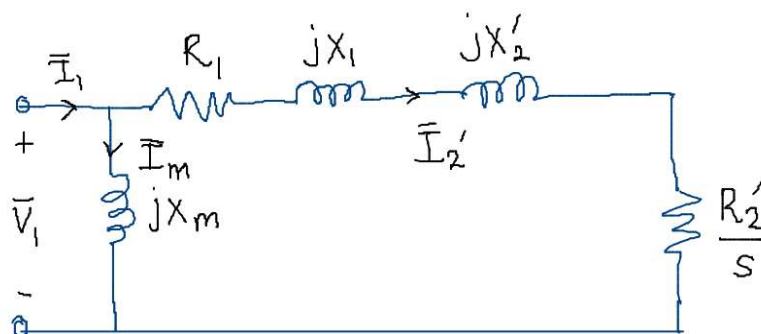
$$P_{in} = \sqrt{3} \cdot V_L \cdot I_L \cdot pf \quad pf := \frac{P_{in}}{\sqrt{3} \cdot V_L \cdot I_L} \quad pf = 0.817 \quad \text{lagging} \quad \text{1 mark}$$

Q4: Induction Machine - Equivalent Circuit Analysis

$$R_1 := 1.4\Omega \quad R_2 := 0.6\Omega \quad X_1 := 2\Omega \quad X_2 := 1\Omega \quad X_m := 50\Omega$$

$$V_L := 415V \quad N_r := 960rpm \quad p := 6 \quad f := 50Hz$$

We use an approximate equivalent circuit. The calculation uses per phase quantities.



Connection Type:
Delta

$$V_1 := V_L \quad V_1 = 415 \text{ V} \quad N_s := \frac{120f}{p} \quad N_s = 1 \times 10^3 \text{ rpm}$$

(a) Under starting condition, i.e. when $s := 1$; **to find line current and power factor**

	mag	phase
$I_2 := \frac{V_1}{R_1 + \frac{R_2}{s} + j \cdot (X_1 + X_2)}$	$ I_2 = 115.1 \text{ A}$	$\arg(I_2) = -56.31 \text{ deg}$
$I_m := \frac{V_1}{j \cdot X_m}$	$ I_m = 8.3 \text{ A}$	$\arg(I_m) = -90 \text{ deg}$
$I_1 := I_2 + I_m$	$ I_1 = 122.093 \text{ A}$	$\arg(I_1) = -58.471 \text{ deg}$

The line current, since the connection is delta, $I_L := \sqrt{3} |I_1|$ $I_L = 211.472 \text{ A}$

The power factor, $\text{pf} = \cos(\theta)$

$\text{pf} := \cos(\arg(I_1))$ $\text{pf} = 0.523$ lagging

3 marks

(b) Under maximum torque condition, i.e. when $s = s_{Tmax}$; **to find the maximum torque**

$$s_{Tmax} := \frac{R_2}{\sqrt{R_1^2 + (X_1 + X_2)^2}} \quad s_{Tmax} = 0.181$$

$$s := s_{Tmax}$$

	mag	phase
$I_2 := \frac{V_1}{R_1 + \frac{R_2}{s} + j \cdot (X_1 + X_2)}$	$ I_2 = 74.309 \text{ A}$	$\arg(I_2) = -32.492 \text{ deg}$
$I_m := \frac{V_1}{j \cdot X_m}$	$ I_m = 8.3 \text{ A}$	$\arg(I_m) = -90 \text{ deg}$
$I_1 := I_2 + I_m$	$ I_1 = 79.078 \text{ A}$	$\arg(I_1) = -37.571 \text{ deg}$

$$P_{ag} := (|I_2|)^2 \frac{R_2}{s} \quad P_{ag} = 18.281 \text{ kW}$$

and $\omega_s := N_s \cdot \frac{2\pi}{60}$

$$T := \frac{P_{ag}}{\omega_s} \quad \text{T} = 174.567 \text{ Nm} \quad \text{per phase}$$

3 marks

(c) Under full load, i.e. when $s := \frac{N_s - N_r}{N_s}$; **to find efficiency at the full-load**

$$s = 0.04$$

	mag	phase
$I_2 := \frac{V_1}{R_1 + \frac{R_2}{s} + j \cdot (X_1 + X_2)}$	$ I_2 = 24.892 \text{ A}$	$\arg(I_2) = -10.366 \text{ deg}$

$I_m := \frac{V_1}{j \cdot X_m}$	$ I_m = 8.3 \text{ A}$	$\arg(I_m) = -90 \text{ deg}$
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$I_1 := I_2 + I_m$	$ I_1 = 27.62 \text{ A}$	$\arg(I_1) = -27.56 \text{ deg}$
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$P_{ag} := (I_2)^2 \cdot \frac{R_2}{s}$	$P_{ag} = 9.294 \text{ kW}$
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$P_m := (I_2)^2 \cdot \frac{R_2}{s} \cdot (1 - s)$	$P_m = 8.922 \text{ kW}$
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$P_{rotational} := 0.275 \text{ kW}$	$P_{out} := P_m - \frac{P_{rotational}}{3}$	$P_{out} = 8.831 \text{ kW}$
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$P_{in} := V_1 \cdot I_1 \cdot \cos(\arg(I_1))$	$P_{in} = 10.161 \text{ kW}$
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Efficiency, $\eta := \frac{P_{out}}{P_{in}} \cdot 100$

$\eta = 86.903$

3 marks